# An Initial Study, the Effect of MgO Addition on Some Physical Properties of Al<sub>2</sub>TiO<sub>5</sub>

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**Abstract**—Aluminium titanate  $(Al_2TiO_5)$  ceramics has excellent refractory properties such as high melting point, low thermal conductivity and good thermal shock resistance. However, instability of  $Al_2TiO_5$  phase and low mechanical strength limit the usage of this material. Some additives are used to overwhelm these problems. In this study, the effects of MgO additions (1.25, 2.5, 5 and 10 by wt. %) on the mechanical strength, bulk density and phase composition of  $Al_2TiO_5$  ceramics was investigated. Equimolar mixtures of  $Al_2O_3$ and TiO<sub>2</sub> with MgO additions were mixed in ethanol medium and samples were formed with uniaxial pressing at 60 MPa with solidstate sintering 1450 °C for 3 hours. The densities of the samples were determined by Archimedes method, mechanical strengths by threepoint bending test, and phase contents by XRD. It was found that the addition of 2.5 wt. % MgO increased the strength of  $Al_2TiO_5$ ceramics by about three times.

*Keywords*— Al<sub>2</sub>TiO<sub>5</sub>, Mechanical Properties, Refractory Ceramics, Sintering.

# I. INTRODUCTION

Aluminium titanate (Al<sub>2</sub>TiO<sub>5</sub>) is a refractory ceramic material, produced by equimolar mixture of Al<sub>2</sub>O<sub>3</sub> and TiO<sub>2</sub> has great potential on high temperature applications. AT ceramics has superior properties, such as high melting point (1860 °C), low thermal conductivity (~1.5 Wm<sup>-1</sup>K<sup>-1</sup>), good thermal shock resistance and resistance to molten aluminum corrosion [1-2]. It is used at molten aluminum industry as a riser tube. There are problems limits the usage of this material.

The first problem is the poor mechanical strength. Microcrack formation occurs during sintering due to the high anisotropy of thermal expansion coefficients of three crystallographic axes. Moreover,  $Al_2TiO_5$  has a pseudobrookite type crystal structure with a theoretical density of 3.70 g/cm<sup>3</sup>. The starting materials  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> and TiO<sub>2</sub> has densities of 3.99 and 4.25 g/cm<sup>3</sup>, respectively. Therefore, formation of Al<sub>2</sub>TiO<sub>5</sub> causes % 11 volume increase [3].

The second problem is the instability of  $Al_2TiO_5$  phase. Al<sub>2</sub>TiO<sub>5</sub> phase tends to decompose with in the temperature range of 800 and 1300 °C [4]. The reason of the decomposition is the collapse of the adjacent  $Al^{3+}$  (0.54 Å) and Ti<sup>4+</sup> (0.67 Å) octahedra because the lattice sites occupied by the Al<sup>3+</sup> ions are too large. The thermal energy available from this collapse allows Al<sup>3+</sup> to migrate, resulting in structural dissolution to rutile and corundum [5]. In order to overwhelm these problems and improve  $Al_2TiO_5$  ceramics properties, researchers have done much work on formation of solid solutions with oxide additives such as MgO or Fe<sub>2</sub>O<sub>3</sub> in to the system which are isomorphous with the mineral pseudobrookite [6-9]. SiO<sub>2</sub>, ZrO<sub>2</sub>, ZrTiO<sub>4</sub> or Mullite is also used to strengthen Al<sub>2</sub>TiO<sub>5</sub> ceramics. These additives do not form solid solutions with Al<sub>2</sub>TiO<sub>5</sub> but inhibit the tendency of Al<sub>2</sub>TiO<sub>5</sub> decomposition [10-11].

In the present work, the effects of MgO additions (1.25, 2.5, 5 and 10 by wt. %) on the mechanical strength, bulk density, and phase composition of  $Al_2TiO_5$  ceramics was investigated.

# II. EXPERIMENTAL PROCEDURE

The raw materials were  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> (>99.7%, 2 µm, Nabaltec), rutile-TiO<sub>2</sub> (>98%, 0.19 µm, TRONOX® 8400), and MgO (>98%, Merck). For the mixtures investigated  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>:TiO<sub>2</sub> rutile was stoichiometric, and the quantity of MgO additive was 1.25, 2.5, 5, and 10% by mass. Powders were mixed in ball mill with porcelain balls using ethanol, and then slurries were dried in an oven at 80 °C for 24 hours. The mixed powders were formed into pellets (diameter of 30 mm and 10 mm thickness) and rectangular bars (80 mm × 15 mm) by uniaxial semi-automatic press with 60 MPa pressure. Subsequently, the green samples were sintered at 1450 for 3 hours in air to obtain dense samples. The amount of additives and sample names are listed in Table 1.

A powder diffractometer with Cu K $\alpha$  radiation ( $\lambda$ =1.5418 Å) and a secondary graphite monochromator were used for the mineralogical analysis. XRD spectra were obtained by scanning from 15° to 70° angles (2 $\theta$ ), with a goniometer speed of 1.25°/min, 40 kV acceleration voltage and 30 mA current.

The bulk density and apparent porosity of the sintered samples were measured with the Archimedes method. The mechanical strengths of the samples were measured by threepoint bending on a computer controlled electronic universal testing machine (Shimadzu, Japan).

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MGO RATIO IN THE EQUIMOLAR MIXTURE OF AL2O3 AND TIO2.	
Sample name	MgO ratio (wt. %)
AT	-
M1	10
M2	5
M3	2.5
M4	1.25

TABLE I

# III. RESULTS AND DISCUSSION

Figure 1 shows the bulk density of the sintered samples with different MgO contents. As it can be seen, MgO content has significant effect on the bulk density. The theoretical density of Al<sub>2</sub>TiO<sub>5</sub> is 3.70 g/cm<sup>3</sup>. Adding 10 wt. % MgO increased the bulk density 3,27 to 3,47 g/cm3. This explains the formation of Al<sub>2</sub>TiO<sub>5</sub> phase and depletion of the starting materials. Adding 2.5 and 5 wt. % MgO has not much effect and both bulk density and apparent porosity. Adding 1.25 wt. % MgO considerably decreased the bulk density and increased the apparent porosity of the samples. Despite the promotion of the Al<sub>2</sub>TiO<sub>5</sub> solid solution formation, 1.25 wt. % MgO addition increased the apparent porosity and decreased the bulk density of the samples. To explain this change, phase content of the samples should be considered.



Figure 3 shows the XRD patterns of the sintered samples with changing the MgO amount. All samples without M4 contained unreacted  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>. Un-doped sample (AT) contained unreacted Al<sub>2</sub>O<sub>3</sub> and TiO<sub>2</sub>, and Al<sub>2</sub>TiO<sub>5</sub>. As the MgO amount increased, the Al<sub>2</sub>TiO<sub>5</sub> peaks became more sharp and intensive, which means Al<sub>2</sub>TiO<sub>5</sub> grains became more crystallized. MgAl<sub>2</sub>O<sub>4</sub> spinel phase formed and TiO<sub>2</sub>-rutile peaks disappeared with just adding 1.25 wt. % MgO. As the MgO content increased MgAl<sub>2</sub>O<sub>4</sub> peaks became stronger. Sample M4 composed of only Al<sub>2</sub>TiO<sub>5</sub> and MgAl<sub>2</sub>O<sub>4</sub> phases. The Al<sub>2</sub>TiO<sub>5</sub> peak at 62 to 64° shifted toward lower 20 values as the MgO amounts were increased. The peak shift indicates the formation of Al<sub>2</sub>TiO<sub>5</sub> solid solution containing MgO, which resulted in lattice expansion [12]. MgO addition promotes the formation of Al<sub>2</sub>TiO<sub>5</sub> and decreaes formation

Al<sub>2</sub>TiO<sub>5</sub> pseudobrookite phase. Figure 4 shows the three-point bending strengths of the samples. Addition of MgO increased the strength with formation solid solution of Al<sub>2</sub>TiO<sub>5</sub>. When MgO exceeds its solubility in Al<sub>2</sub>TiO<sub>5</sub>, it forms MgAl<sub>2</sub>O<sub>4</sub>. It is well known that formation of MgAl<sub>2</sub>O<sub>4</sub> at the grain boundaries limits the grain growth of Al<sub>2</sub>TiO<sub>5</sub> and increases mechanical properties. Despite of increase at the bulk density and decrease of the apparent porosity with addition of MgO, mechanical properties of sintered samples did not increased after adding 2.5 wt. %. The problem was macro-crack formation after sintering of the samples due to densification inhomogeneity arising from uniaxial pressing. Cold isostatic pressing could be a solution to produce more dense and homogenous samples without cracks.

temperature of Al<sub>2</sub>TiO<sub>5</sub>. Also, it stabilizes solid solution of



Fig. 4 Fracture strength of the sintered samples

Fig. 2 Apparent porosity of the sintered samples

MB

Sample

M2

M1

M4

2 Ð

AT



Fig. 3 X-ray diffraction patterns of the sintered samples: AT, M1, M2, M3 and M4. T is  $Al_2TiO_5$ , C is  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>, R is TiO<sub>2</sub>-rutile and S is  $Mg_2AlO_4$  spinel

# IV. CONCLUSION

In this study, MgO-doped  $Al_2TiO_5$  ceramics were produced from  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>-rutile and MgO. MgO promoted formation of Al<sub>2</sub>TiO<sub>5</sub> and increased strength with the minimum addition of 2.5 wt. %.

2.5 wt. % MgO addition formed  $MgAl_2O_4$  spinel and increased the three-point bending strength of the  $Al_2TiO_5$  ceramics by nearly three times.

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